

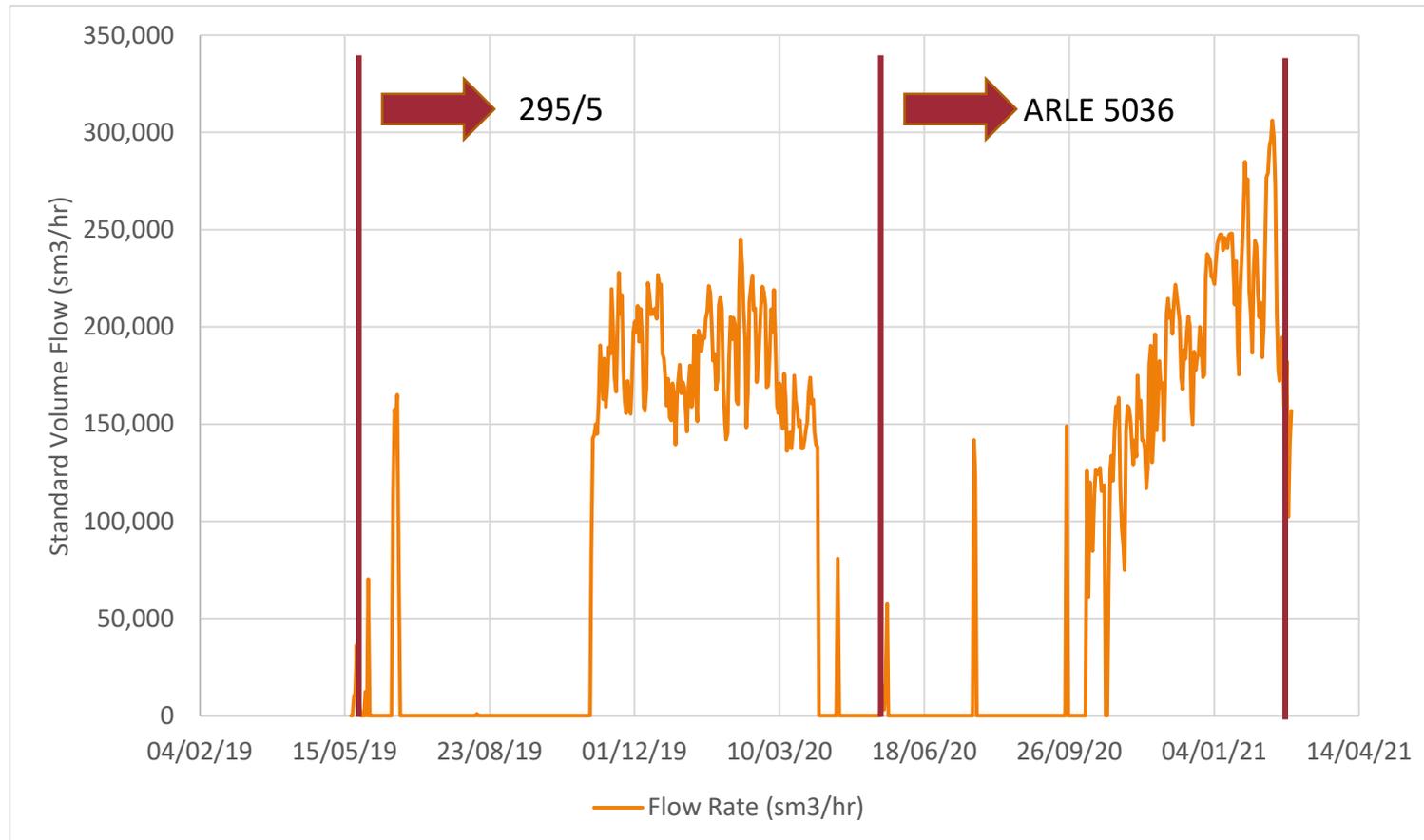
**MEASUREMENT ERROR &
CALCULATION METHODOLOGY**

**ALREWAS EM MER
EM009**



**PAUL DANIEL
I-VIGILANT TECHNOLOGIES LIMITED**

ALREWAS MEASUREMENT ERROR REPORT



- Plate installed backwards
 - 23rd May 2019
- Plate swapped out and installed backwards
 - 20th May 2020
- Plate swapped out and installed correctly
 - 23rd Feb 2021

MEASUREMENT ERROR OCCURRED FROM
23RD MAY 2019 TO 23RD FEB 2021



DETERMINATION OF MEASUREMENT ERROR

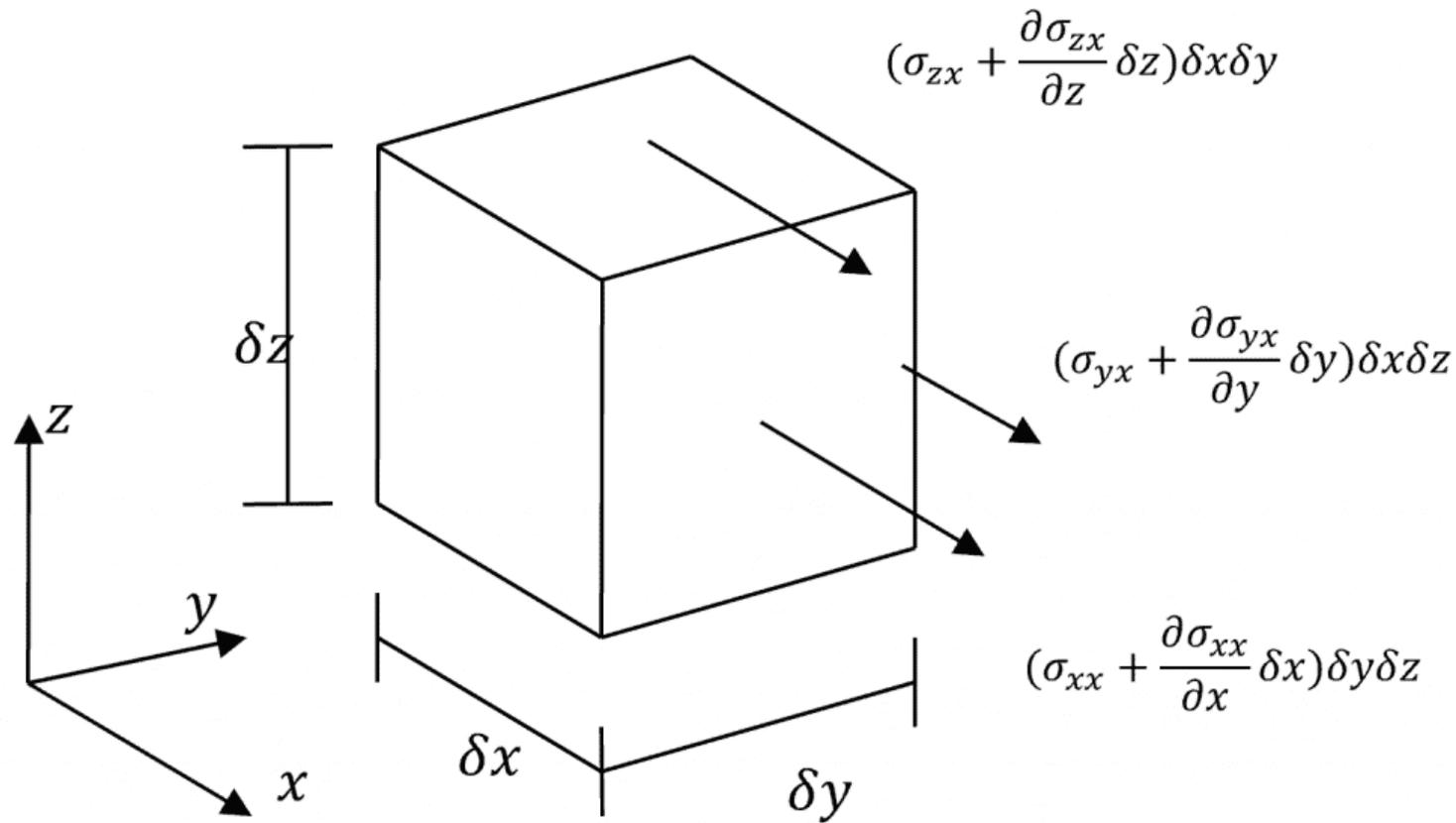
Computational Fluid Dynamics (CFD)

- A high level of expertise is required to set the problem up properly
- Configuration of the geometry
- Configuration of the mesh
- Selection of boundary conditions
- Solver constraints and convergence criteria
- What is the uncertainty associated with the result?

Flow Testing Using a Clamp-on Ultrasonic

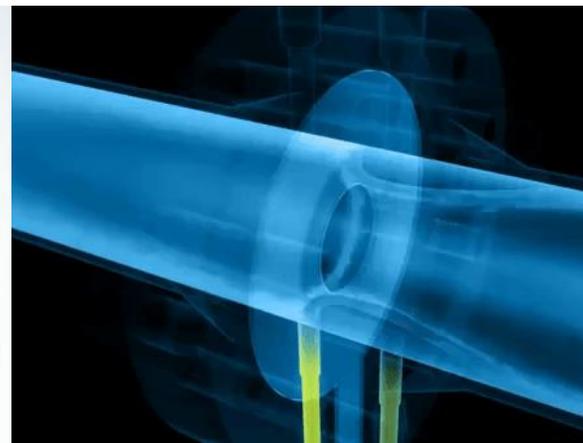
- How well do clamp-on meters work ok in gas?
- How accurately can the pipe diameter be determined?
- How accurately can the pipe wall thickness be determined?
- How repeatable/reproducible is the flow meter?
- Can constant flow be maintained for the testing?
- What is the uncertainty of the measurement?

BOTH CFD AND FLOW TESTING WAS PERFORMED



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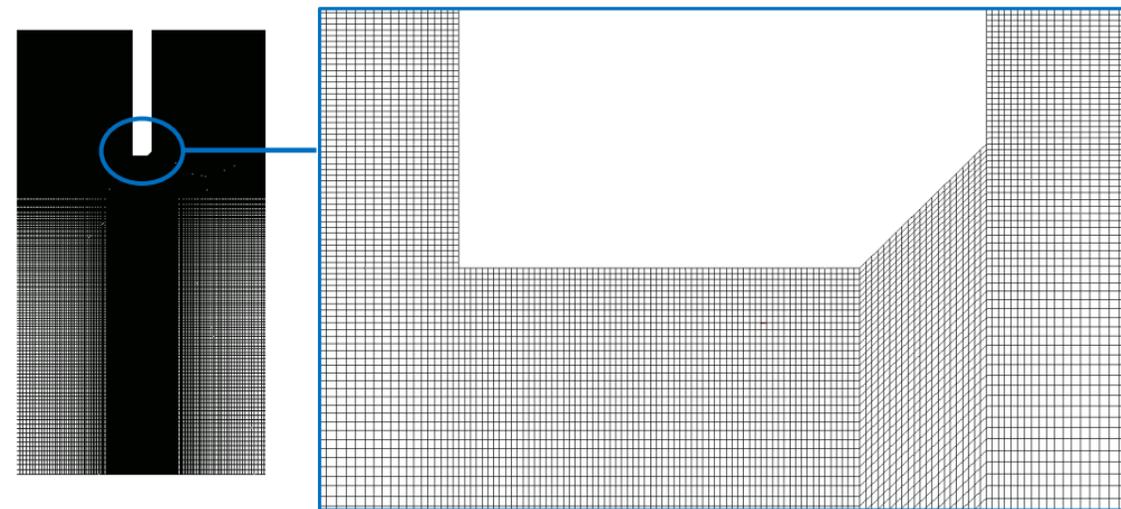
| MASS | ACCELERATION | FORCE |
|----------------------|---------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|
| ρ | $\left(\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right)$ | $\rho \vec{g} - \nabla p + \mu \cdot \nabla^2 \vec{v}$ |
| Density of the Fluid | Change in Velocity over Time Speed and Direction of Fluid | External Forces such as Gravity Pressure Gradient Internal Stress Forces (viscous effects) |



Computational Fluid Dynamics

DETERMINATION OF MEASUREMENT ERROR USING CFD

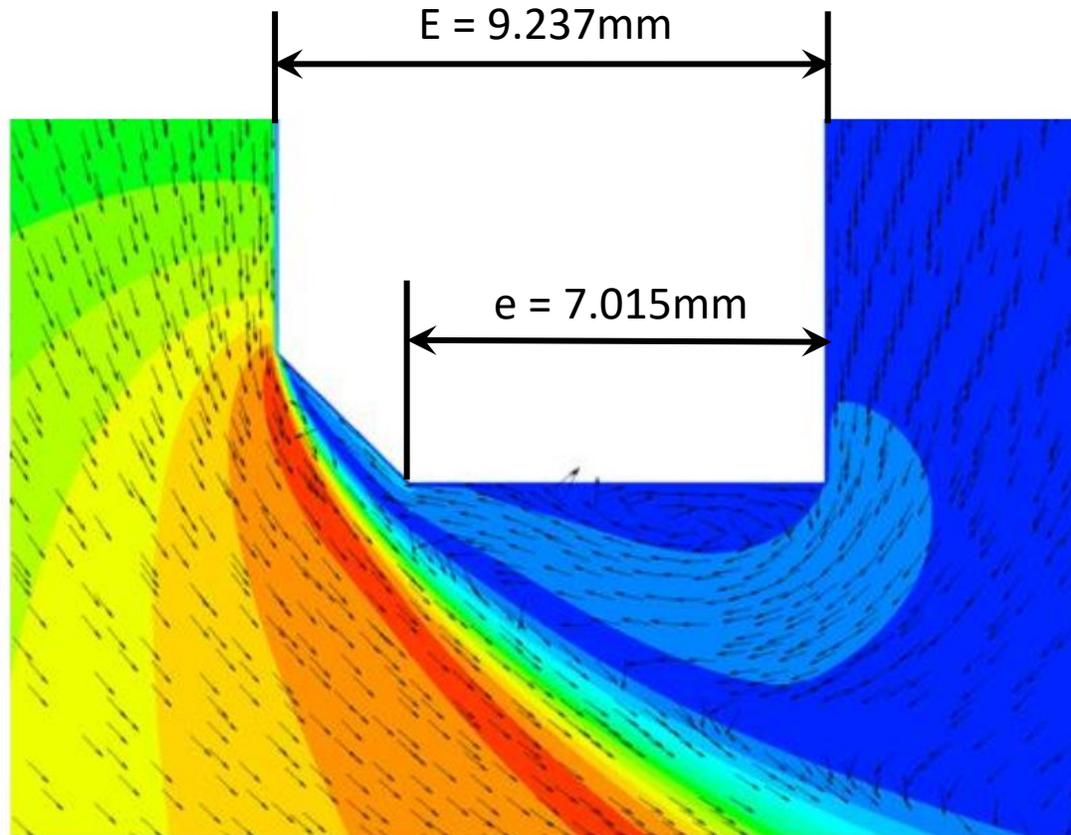
- Simulated 2 orifice plates, forward and reverse at 3 Reynolds No.
 - Non-structural hexahedral mesh
 - Mesh of 994,900 nodes - 500,000 elements
 - Reynolds-Averaged Navier-Stokes (RANS) based model
 - $k-\omega$ Shear Stress Transport (SST)
 - Turbulent flows
 - Accurately predicts flow separation
 - Two solvers used
 - ANSYS CFX
 - ANSYS Fluent



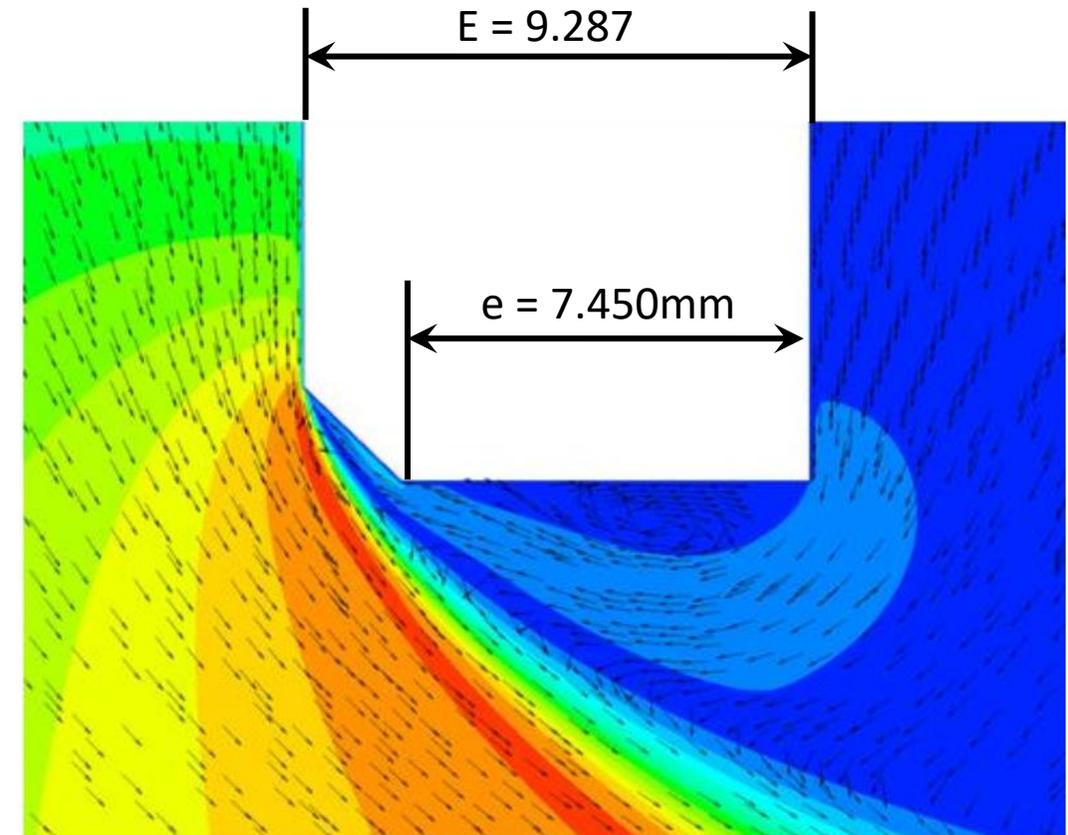
Low
Pressure



High
Pressure



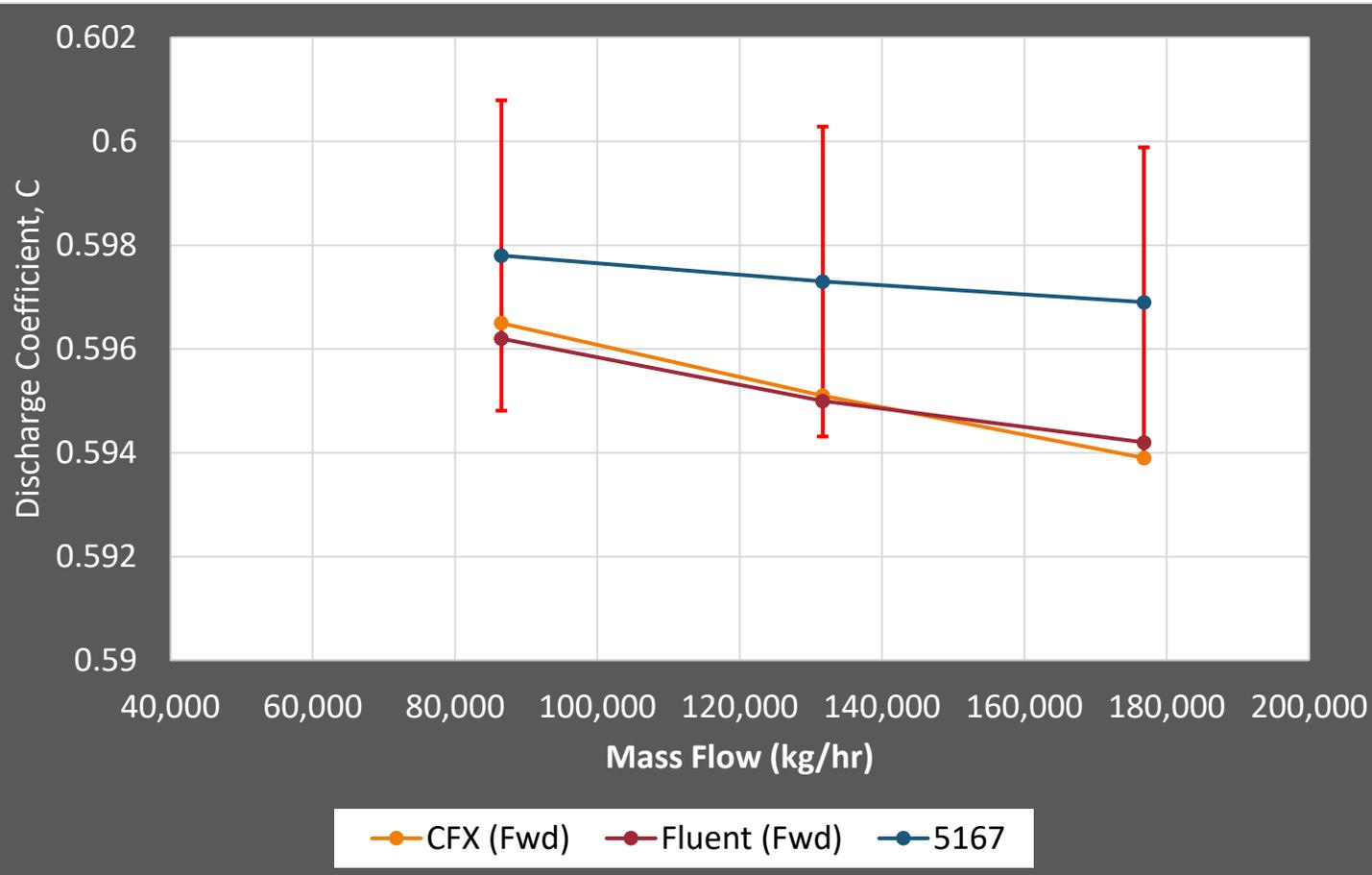
295/5, $d=309.997$



ARLE 5036, $d=310.002$

VERY SIMILAR ORIFICE PLATES. DIFFERENCE IN $d=0.005\text{mm}$

CFD VALIDATION

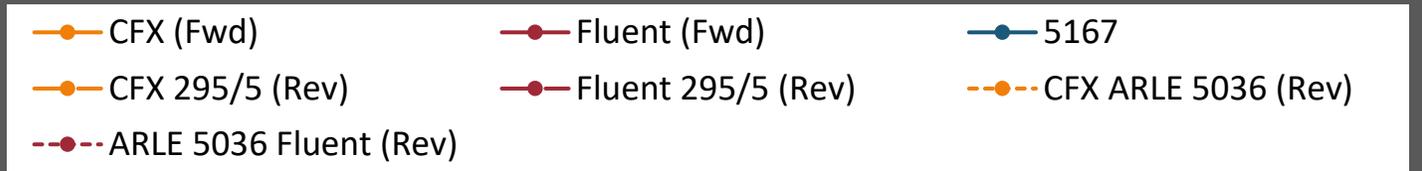
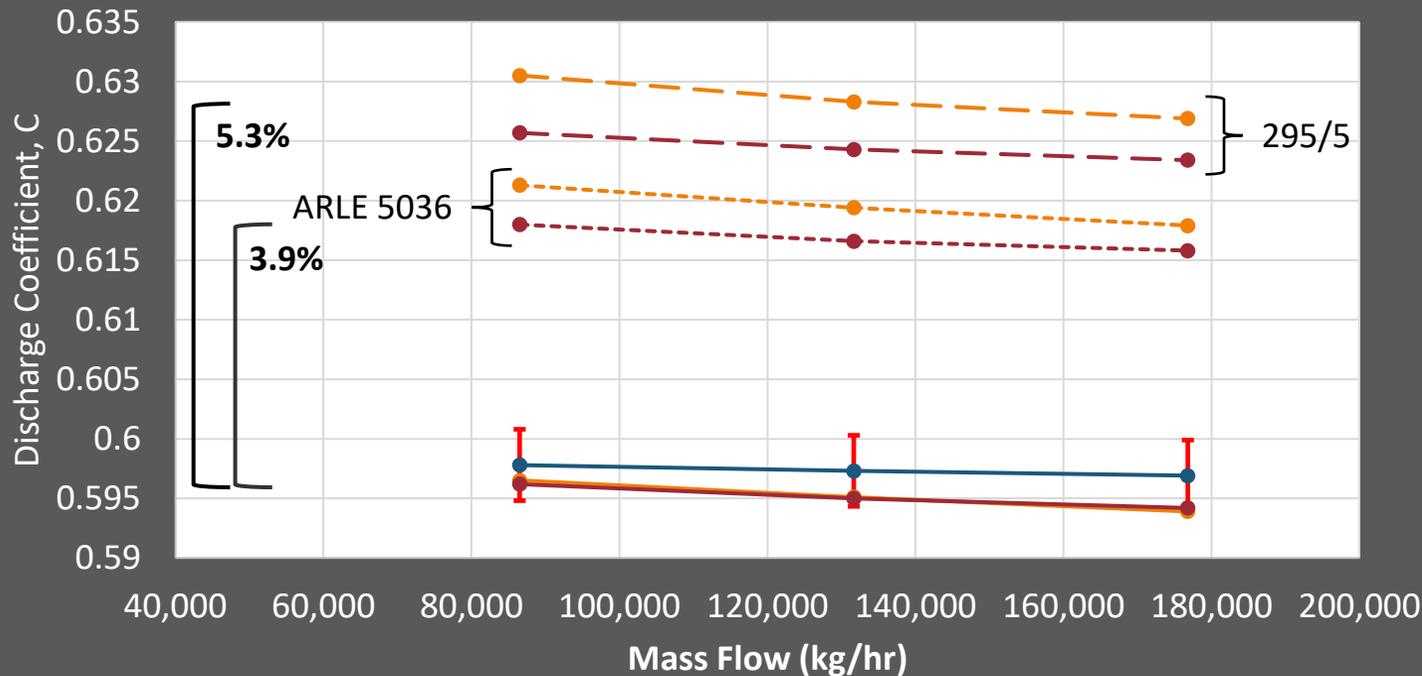


| Flow (kg/hr) | CFX (Fwd) | Fluent (Fwd) | ISO 5167 | Error (%) |
|--------------|-----------|--------------|----------|-----------|
| 86,519 | 0.5965 | 0.5962 | 0.5978 | -0.27% |
| 131,659 | 0.5951 | 0.595 | 0.5973 | -0.39% |
| 176,799 | 0.5939 | 0.5942 | 0.5969 | -0.45% |

- 5167 Error Bands – 0.5%
- CFD conducted at 3 points
- Simulated in correct orientation
- All CFD results with 0.5% of ISO5167
- Results for plate 295/5
- Both plates provided very similar results

CFD DISCHARGE COEFFICIENT CLOSE TO ISO 5167

CFD REVERSE ORIENTATION



| Flow (kg/hr) | CFX 295/5 | Fluent 295/5 | CFX ARLE 5036 | Fluent ARLE 5036 |
|--------------|-----------|--------------|---------------|------------------|
| 86,519 | 0.6305 | 0.6257 | 0.6213 | 0.618 |
| 131,659 | 0.6283 | 0.6243 | 0.6194 | 0.6166 |
| 176,799 | 0.6269 | 0.6234 | 0.6179 | 0.6158 |

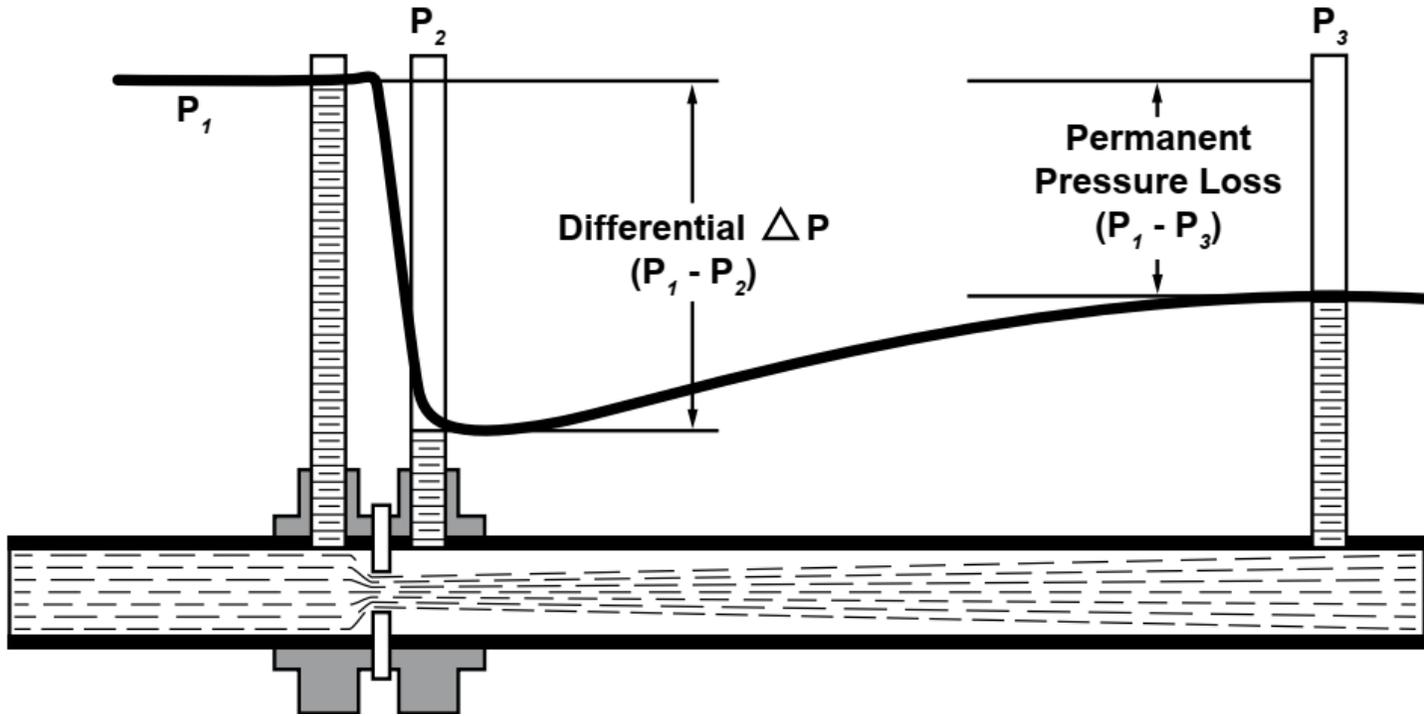
- Both plates had an increased C
- Under measurement predicted
- 295/5 has larger under measurement
- CFX predicts slightly larger error

$$q_r = \frac{C}{\sqrt{1 - \beta^4}} \frac{\pi d^2}{4} \varepsilon \sqrt{2\Delta P_r \rho}$$

$$C_r \varepsilon_r = \frac{4q_m \sqrt{1 - \beta^4}}{\pi d^2 \sqrt{2\Delta P_r \rho}}$$

$$q_m = q_r \frac{C_r \varepsilon_r}{C \varepsilon}$$

UNDER MEASUREMENT OF 4-5% PREDICTED



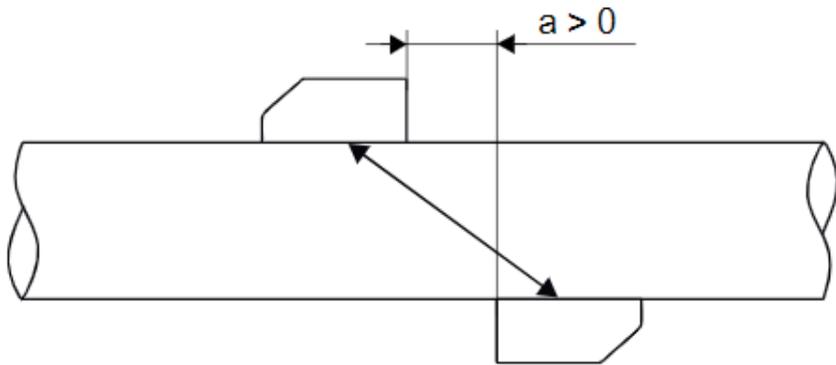
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Flow Tests

DETERMINATION OF MEASUREMENT ERROR USING FLOW TESTS

- Clamp-on Ultrasonic Flowmeter
 - Installed $>5D$ upstream of Orifice
 - Pipe wall thickness measured by ultrasonic thickness gauge
 - Pipe circumference measured by tape
 - USM recommends separation of transducers
 - Run with Plate in correct orientation – determine ‘meter factor’
 - Run with both plates in reverse orientation to determine meter error in reverse orientation
 - Run second plate in correct orientation to determine reproducibility of USM



FLOW TEST 1

295/5 FORWARD

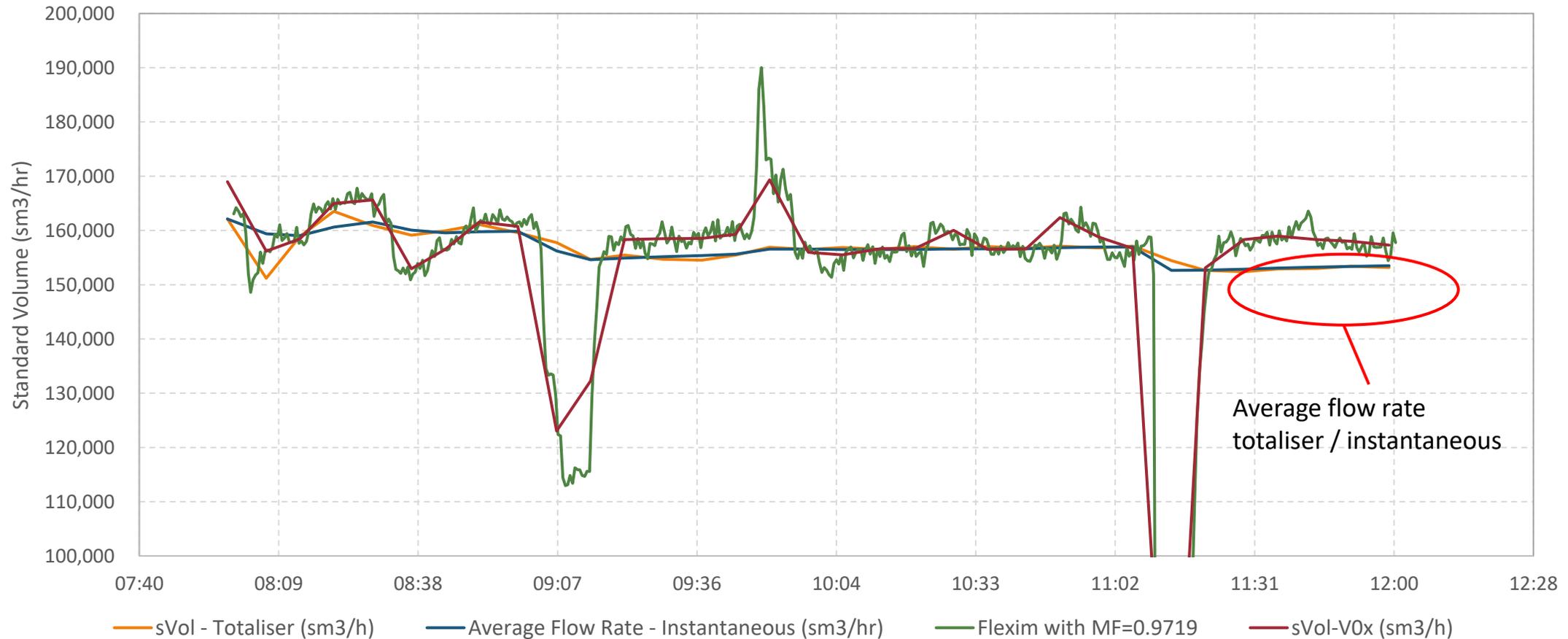


PLATE 295/5 IN THE CORRECT ORIENTATION
METER FACTOR FOR USM = 0.9719

FLOW TEST 2

295/5 REVERSE

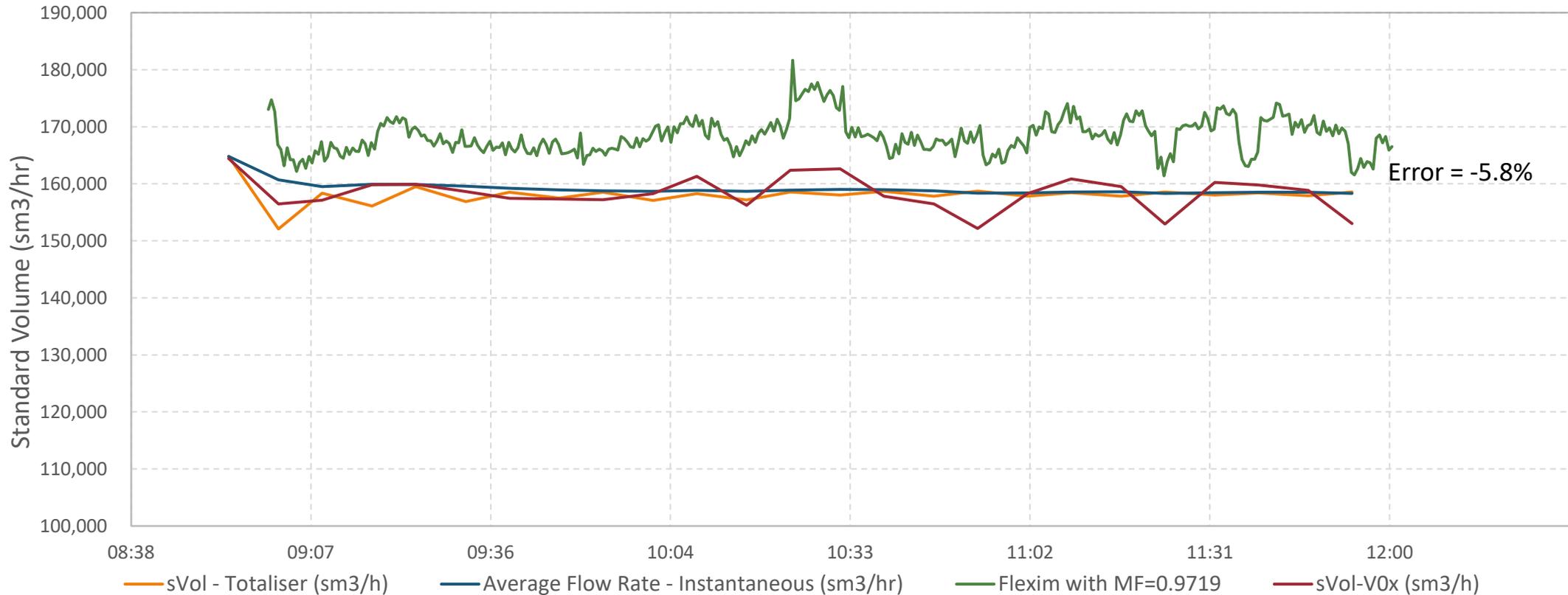


PLATE 295/5 IN THE REVERSE ORIENTATION

ORIFICE METER READS 5.8% LOWER THAN THE MF CORRECTED USM

FLOW TEST 3

ARLE 5036 FORWARD



ORIFICE METER READS 0.025% LOWER THAN THE MF CORRECTED USM
USM DEMONSTRATED TO BE REPRODUCIBLE

FLOW TEST 4

ARLE 5036 REVERSE

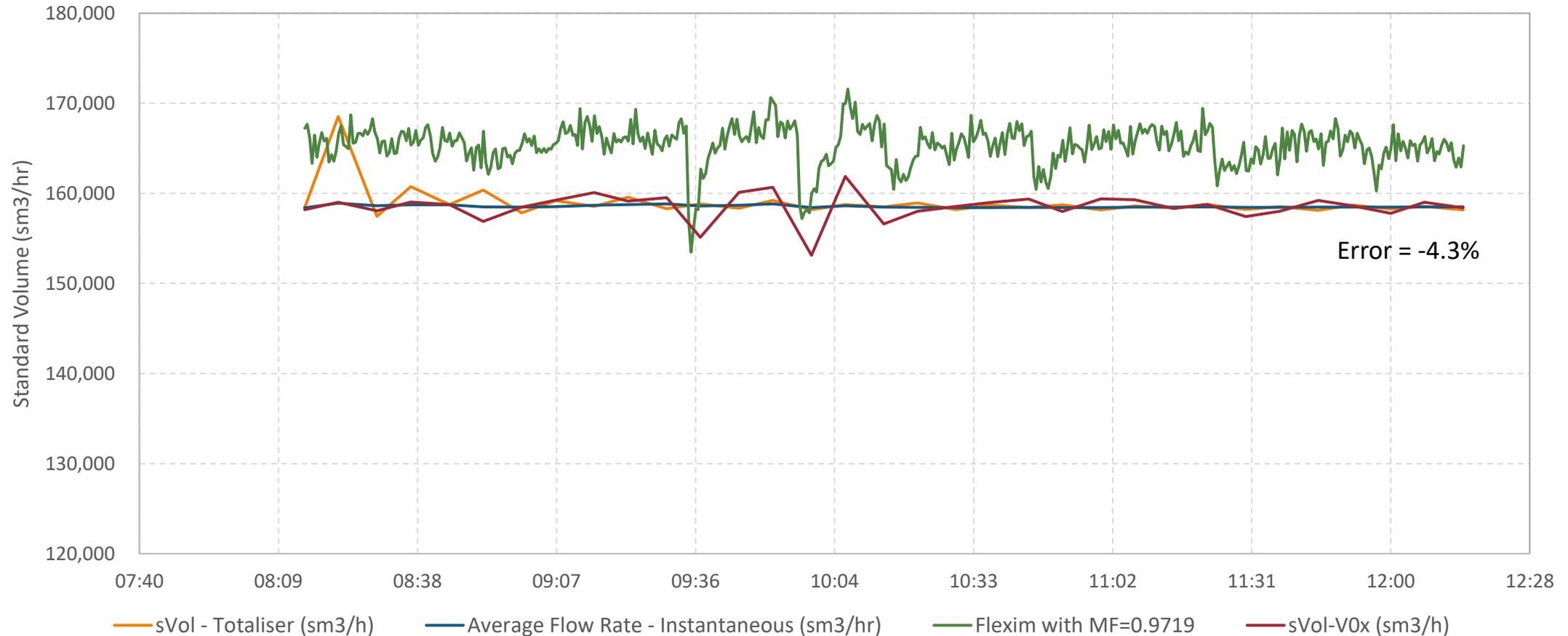
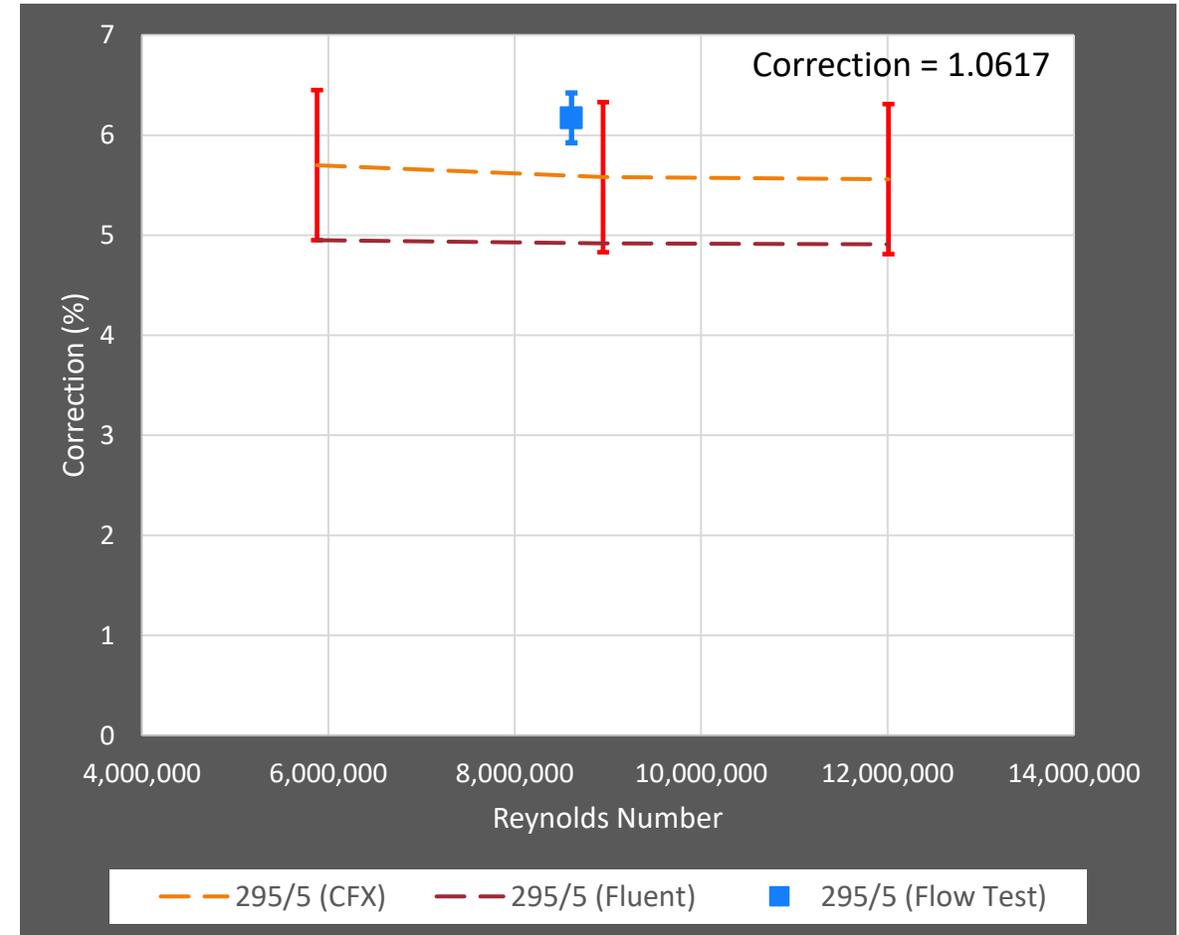
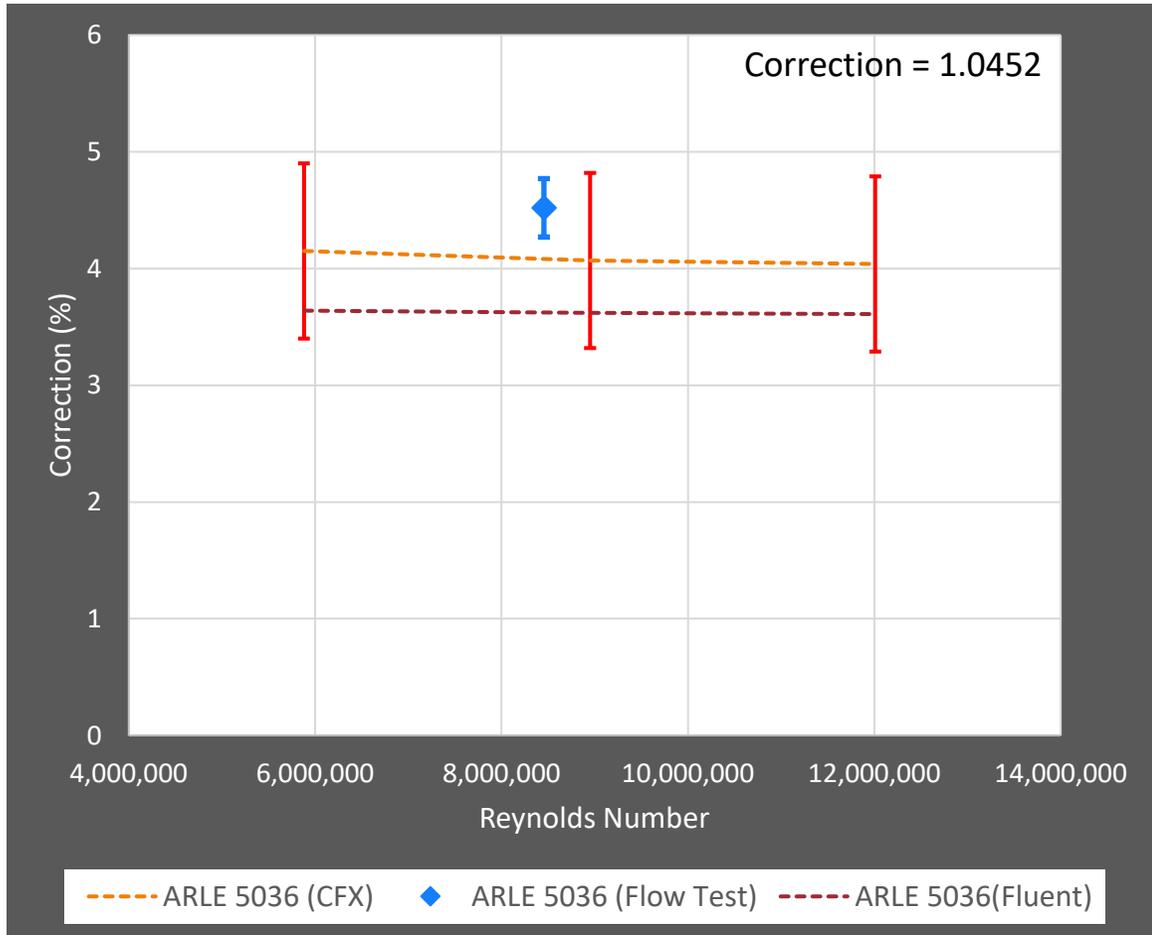


PLATE ARLE 5036 IN THE REVERSE ORIENTATION
ORIFICE METER READS 4.3% LOWER THAN THE MF CORRECTED USM

RESULT SUMMARY



ERROR BARS 0.75% FROM CFX, 0.25% FROM FLOW TEST

IF YOUR EXPERIMENT NEEDS STATISTICS, YOU SHOULD HAVE DONE A BETTER EXPERIMENT....

MIS-MEASUREMENT SUMMARY

| | |
|----------------------------------------------------------|--------------------|
| Site Name: | Alrewas EM MTD |
| DN Reference: | MER/CAD/204/21 |
| Measurement Error Notification: | EM009 |
| Meter Type: | Orifice Meter |
| LDZ: | EM |
| Start Date of Measurement Error: | 23/05/2019 |
| End Date of Measurement Error: | 23/02/2021 |
| Throughput during Period – Standard Volume (sm3): | 1,319,252,002 |
| Throughput during Period – Energy (kWh): | 14,395,996,944 |
| Over or Under Measurement: | Under measurement |
| Correction – Standard Volume, sm3 / (%): | 71,113,997 (5.4%) |
| Correction – Energy, kWh (%): | 776,099,094 (5.4%) |



5.4% MEASUREMENT ERROR OVER FULL PERIOD

THANK YOU

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